Towards the optimization of a domestic-scale organic Rankine cycle system for combined heating and power provision in the UK

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PhD project aims

To assess the potential to provide combined heating and power from small-scale solar thermal technology in the United Kingdom

To design and model a domesticscale system based on ORC technology and powered by heat from a roof-top solar collector array

To investigate the most suitable system components based on the size of the system and the nature of the UK solar resource



Conventional domestic solar technologies

Consider a 15 m² roof



- Cover with PV (MC-Si) at ≈ € 5200 (system cost including inverter + install)
- Electrical power output ≈ 1750 kWh_e/yr
 ≈ 200 We_(avg) (50% electricity demand)
- Annual electricity bill savings (up to) 270 €/year

- Assuming 25 year system life and annual running cost = 1% of capital cost.
- Typical performance and demand figures taken from DECC and The Energy Saving Trust.

Conventional domestic solar technologies

Consider a 15 m² roof



Solar hot water option (evacuated tube):

- System cost: 5 m² / 30 tube collector array + cylinder + plumbing + install ≈ € 4500
- Hot water provision ≈ 1450 kWh_{th}/year
 ≈ 60 litres hot water per day (50% of demand)
- Annual savings on gas bill ≈ 75 €/year
- Assuming 25 year system life and annual running cost = 1% of capital cost.
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Cover remaining 70% with PV PV system cost. 10 m² ≈ € 4000

Electrical power output $\approx 1150 \text{ kWh}_{e}/\text{year}$ (130 We_{avg}) $\approx 35\%$ electricity demand

Electricity bill savings ≈ 180 €/year

Total energy bill savings ≈ 255 €/year

Solar-ORC system

Consider a 15 m² roof



Solar thermal heat and power system

- Entire roof covered with solar thermal collectors
- Power generation via an ORC engine
- Cost of ORC components + install + additional collectors ≈ € 3000
- Power generation in the region of 700-950 kWh/yr (80-110 We average)
 ≈ up to 30% demand
- 90-140 €/year electricity bill savings

- Assuming 25 year system life and annual running cost = 1% of capital cost.
- Typical demand figures taken from DECC.

Previous work – developing a system model

- Initial configuration: indirect heating of ORC up-stream of hot water generator
- Simple component sub-models
- R245fa working fluid
- Fixed fluid flow-rates
- 15 m² solar collector array area
- London solar irradiance data
- Demand profiles for domestic electricity and hot water use
- Assumed that heat rejection is to mains water at fixed temperature (10°C)



Collector comparison

- Non-concentrating <u>evacuated tube</u> collector at fixed orientation due south and 36° tilt angle
- Concentrating <u>parabolic trough</u> collector with perfect 2-axis solar tracking
- Collectors modelled using manufacturers efficiency curves
- Semi-optimized for fixed flow-rates and simulated over an annual period

Results of annual simulation with ORC model:

- Evacuated tube ORC system: 588 kWh/year (67 We_{avg})
- Parabolic trough ORC system: 657 kWh/year (75 We_{avg})





Solar collector selection



Calculation of maximum power

Maximum power = exergy flow at collector outlet:



Solar collector maximum work



Maximum power output: (peak irradiance)

Evacuated tube 120 W/m² (reversible) and 65 W/m² (endoreversible) at 270 °C outlet temperature. Parabolic trough 240 W/m² (reversible) and 145 W/m² (endoreversible) at 550 °C outlet temperature.

Annual maximum work (15 m² evacuated tube array):

590–993 kWh (67-113 $\rm W_{\rm avg}),$ endoreversible

Freeman et al. (2013)

Controlling for optimum temperatures



Model variants

Initial fixed flow-rate model:

- Modelled using "time-marching" approach
- Exiting temperature for interval (i) becomes the initial temperature in interval (i+1)



 $T_{\rm sc,in(i+1)} = T_{\rm sc,in(i)} + (\dot{Q}_{\rm sc(i)} - \dot{Q}_{\rm ORC(i)} - \dot{Q}_{\rm hwc(i)})/\dot{m}_{(i)}c_{\rm p}$

Fixed pressures and flow rates: $P_{\rm evap}$ = 10 bar, $\dot{m}_{\rm sc}$ = 0.03 kg/s, $\dot{m}_{\rm wf}$ = 0.01 kg/s, 150 Temperature [∘C] 100 T_{sc.in} 50 T_{sc,out} T_{wf,evap} 0 8 10 12 14 16 18 6 400 DRC work output [W] 300 200 100 0 8 12 6 10 14 16 18

Time [hour]

Model variants

Variable flow-rate model:

- Modelled using a "quasi-equilibrium" approach
- Temperatures in the system are solved for an equilibrium state for each time interval



Fixed pressures and collector flow rate: <u>Variable</u> ORC working fluid flow rate.



Controlling for optimum temperatures

Starting point:

- Initial inlet temperature
- Environmental parameters known
- ORC condensation temperature/pressure (State 1) is known



Controlling for optimum temperatures

Starting point:

- Initial inlet temperature
- Environmental parameters known
- ORC condensation temperature/pressure (State 1) is known
- Find the collector outlet temperature and flow rate corresponding to maximum exergy output for given $T_{\rm sc,in}$, $T_{\rm ext}$ and G

Input variables: $T_{\rm sc,in}, G, T_{\rm ambient}, T_0$ 0.3 *T*_{sc,out,optimum} 0.25 $\dot{m}_{
m sc,optimum}$ $\dot{X}_{
m sc,out}$ 0.2 0.15 0.1 0.05 $T_{\rm sc,in}$ 0 200 300 0 100 400 500

T_{sc,out}

Controlling for optimum temperatures

- Choose initial T_{sc,in}
- Set optimal T_{sc,out}



Controlling for optimum temperatures

- Choose initial *T*_{sc,in}
- Set optimal T_{sc,out}
- Calculate T_3 and \dot{m}_{wf}
- Try higher values of *P*_{evap} until pinch limit reached
- Calculate power output from ORC engine.



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- Set optimal *T*_{sc,out}
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- Choose a new $T_{\rm sc,in}$



Controlling for optimum temperatures

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- Calculate power output from ORC engine.
- Choose a new T_{sc,in}
- Repeat calculation procedure until W is maximised



Optimal performance region



Optimal performance region



Results (annual average day)



- Mean day work output = 1.9 kWh/day = 79 W average
- 16.5% increased power output compared to system where only working fluid flow rate is varied

Results (annual average day)



Conclusions

- Domestic heat and power systems based on solar-ORC technology have the potential to be a versatile and cost-effective alternative to conventional PV and solar hot water systems
- Modulation of system flow-rates and evaporation pressure has demonstrated an increase in the power output of the system under variable (solar) heat input
- A methodology has been proposed for calculating the maximum power settings based on exergy analysis of the solar collector
- Cost and practicality limitations are to be considered for implementation in a real control strategy

Thank you

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